

Vehicle Propulsion Systems

Lecture 3

Conventional Powertrains with Transmission
Performance, Tools and Optimization

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About the hand-in tasks

- General advice
 - Prepare yourselves before you go to the computer
 - Make a plan (list of tasks)
- Hand-in Format
 - Electronic hand-in
 - Report in PDF-format
 - Reasons:
 - Easy for us to comment
 - Will give you fast feedback

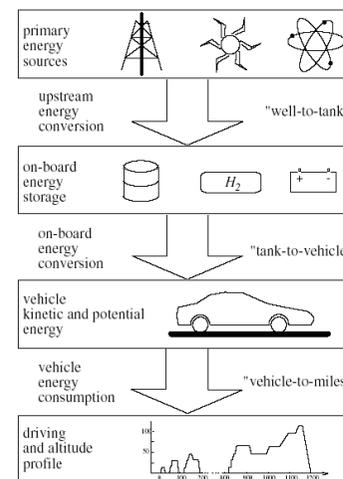
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Outline

- 1 Repetition
- 2 Gear-Box and Clutch Models
 - Selection of Gear Ratio
 - Gear-Box Efficiency
 - Clutches and Torque Converters
- 3 Analysis of IC Powertrains
 - Average Operating Point
 - Quasistatic Analysis
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 - Performance and Driveability
- 5 Optimization Problems
 - Gear ratio optimization
 - Software tools

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Energy System Overview



Primary sources

Different options for on-board energy storage

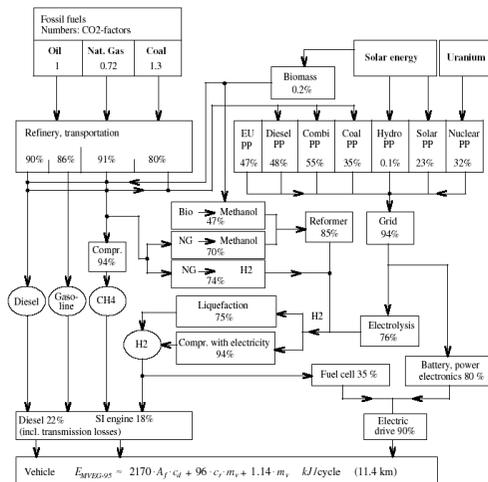
Powertrain energy conversion during driving

Cut at the wheel!

Driving mission has a minimum energy requirement.

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W2M – Energy Paths

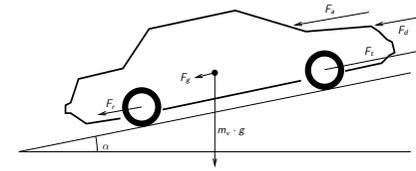


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The Vehicle Motion Equation

Newtons second law for a vehicle

$$m_v \frac{d}{dt} v(t) = F_t(t) - (F_a(t) + F_r(t) + F_g(t) + F_d(t))$$



- F_t – tractive force
- F_a – aerodynamic drag force
- F_r – rolling resistance force
- F_g – gravitational force
- F_d – disturbance force

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Mechanical Energy Demand of a Cycle

Only the demand from the cycle

- The mean tractive force during a cycle

$$\bar{F}_{trac} = \frac{1}{x_{tot}} \int_0^{x_{tot}} \max(F(x), 0) dx = \frac{1}{x_{tot}} \int_{t \in trac} F(t)v(t)dt$$

where $x_{tot} = \int_0^{t_{max}} v(t)dt$.

- Note $t \in trac$ in definition.
- Only traction.
- Idling not a demand from the cycle.

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Evaluating the integral

Tractive force from *The Vehicle Motion Equation*

$$F_{trac} = \frac{1}{2} \rho_a A_f c_d v^2(t) + m_v g c_r + m_v a(t)$$

$$\bar{F}_{trac} = \bar{F}_{trac,a} + \bar{F}_{trac,r} + \bar{F}_{trac,m}$$

Resulting in these sums

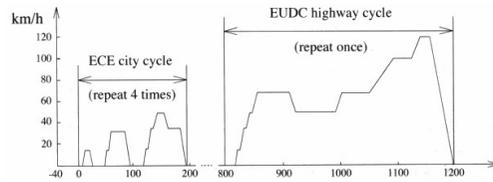
$$\bar{F}_{trac,a} = \frac{1}{x_{tot}} \frac{1}{2} \rho_a A_f c_d \sum_{i \in trac} \bar{v}_i^3 h$$

$$\bar{F}_{trac,r} = \frac{1}{x_{tot}} m_v g c_r \sum_{i \in trac} \bar{v}_i h$$

$$\bar{F}_{trac,m} = \frac{1}{x_{tot}} m_v \sum_{i \in trac} \bar{a}_i \bar{v}_i h$$

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Values for cycles



Numerical values for the cycles:

{MVEG-95, ECE, EUDC}

$$\bar{X}_{trac,a} = \frac{1}{X_{tot}} \sum_{i \in trac} \bar{v}_i^3 h = \{319, 82.9, 455\}$$

$$\bar{X}_{trac,r} = \frac{1}{X_{tot}} \sum_{i \in trac} \bar{v}_i h = \{0.856, 0.81, 0.88\}$$

$$\bar{X}_{trac,m} = \frac{1}{X_{tot}} \sum_{i \in trac} \bar{a}_i \bar{v}_i h = \{0.101, 0.126, 0.086\}$$

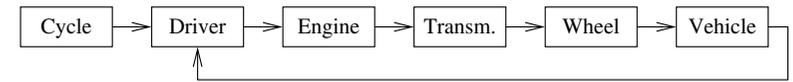
Adopting appropriate units and packaging the results as an Equation

$$\bar{E}_{MVEG-95} \approx A_f c_d 1.9 \cdot 10^4 + m_v c_r 8.4 \cdot 10^2 + m_v 10 \quad kJ/100km$$

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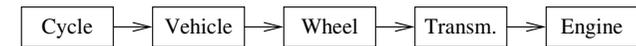
Two Approaches for Powertrain Simulation

- Dynamic simulation (forward simulation)



- "Normal" system modeling direction
- Requires driver model

- Quasistatic simulation (inverse simulation)

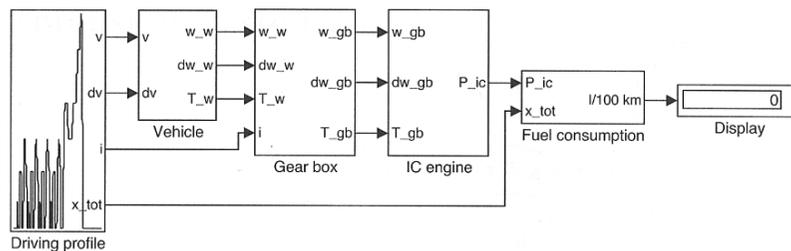


- "Reverse" system modeling direction
- Follows driving cycle exactly

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QSS Toolbox – Quasistatic Approach

- IC Engine Based Powertrain



- The Vehicle Motion Equation – With inertial forces:

$$\left[m_v + \frac{1}{r_w^2} J_w + \frac{\gamma_e^2}{r_g^2} J_e \right] \frac{d}{dt} v(t) = \frac{\gamma_e}{r_w} T_e - (F_a(t) + F_r(t) + F_g(t) + F_d(t))$$

- Gives efficient simulation of vehicles in driving cycles

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Different Types of Gearboxes

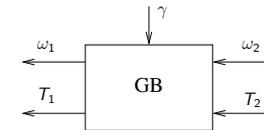
- Manual Gear Box
- Automatic Gear Box, with torque converter
- Automatic Gear Box, with automated clutch
- Automatic Gear Box, with dual clutches (DCT)
- Continuously variable transmission

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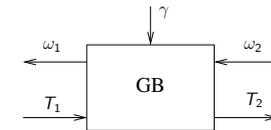
Causality and Basic Equations

- Causalities for Gear-Box Models

Quasistatic Approach



Dynamic Approach



- Power balance – Loss free model

$$\omega_1 = \gamma \omega_2, \quad T_1 = \frac{T_2}{\gamma}$$

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Connections of Importance for Gear Ratio Selection

- Vehicle motion equation:

$$m_v \frac{d}{dt} v(t) = F_t - \frac{1}{2} \rho_a A_f c_d v^2(t) - m_v g c_r - m_v g \sin(\alpha)$$

Constant speed $\frac{d}{dt} v(t) = 0$:

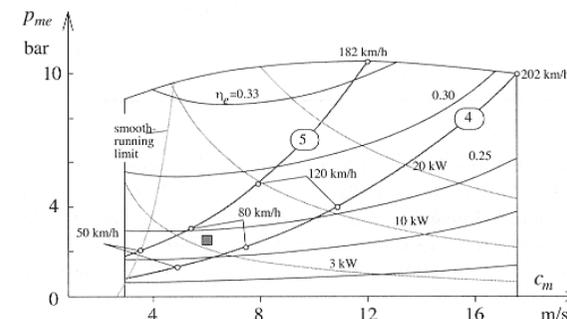
$$F_t = \frac{1}{2} \rho_a A_f c_d v^2(t) + m_v g c_r + m_v g \sin(\alpha)$$

- A given speed v will require power $F_t v$ from the powertrain.
- This translates to power at the engine $T_e \omega_e$.
Changing/selecting gears decouples ω_e and v .
- Required tractive force increases with speed.
For a fixed gear ratio there is also an increase in required engine torque.

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Selection of Gear Ratio – Engine Centric View

Gear ratio selection connected to the engine map.



The gear ratio, maps the road load into the engine map

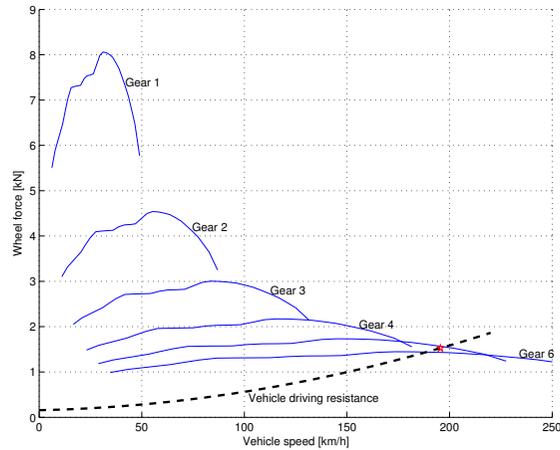
Selecting gear ratios helps achieve goals

- Top speed = Gear 4
- Overdrive = Gear 5 (F.E.)

Additionally: Also geometric ratio between gears. $\frac{i_{g,1}}{i_{g,2}} \approx \frac{i_{g,2}}{i_{g,3}} \approx \frac{i_{g,3}}{i_{g,4}} \approx \frac{i_{g,4}}{i_{g,5}}$

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Selection of Gear Ratio – Road Centric View



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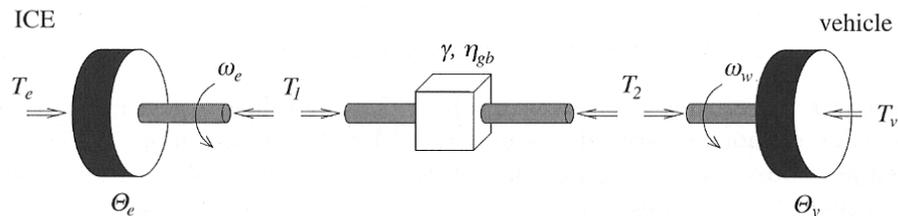
Selection of Gear Ratio

Optimizing gear ratio for a certain cycle.

- Potential to save fuel.
- Case study 8.1 (we'll look at it later).

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Gear-box Efficiency



- In traction mode

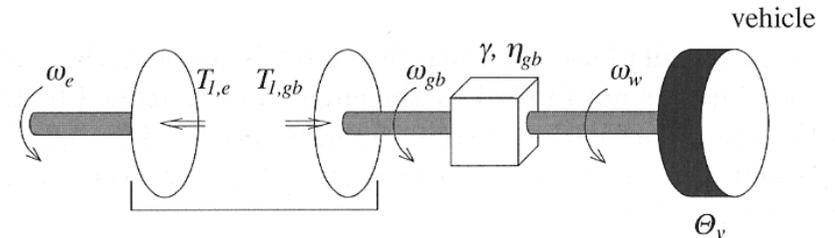
$$T_2 \omega_w = e_{gb} T_1 \omega_e - P_{0,gb}(\omega_e), \quad T_1 \omega_e > 0$$

- In engine braking mode (fuel cut)

$$T_1 \omega_e = e_{gb} T_2 \omega_w - P_{0,gb}(\omega_e), \quad T_1 \omega_e < 0$$

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Clutch and Torque Converter Efficiency



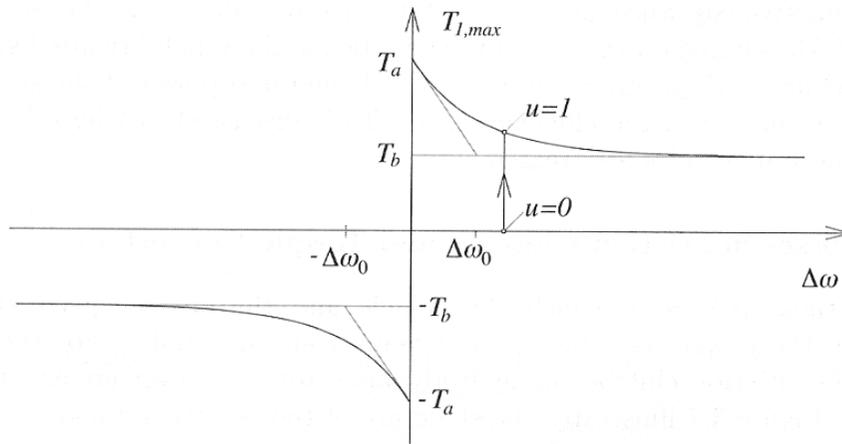
Friction clutch torque:

$$T_{1,e}(t) = T_{1,gb}(t) = T_1(t) \forall t$$

Action and reaction torque in the clutch, no mass.

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Torque Characteristics of a Friction Clutch



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Approximation of the maximum torque in a friction clutch

$$T_{1,max} = \text{sign}(\Delta\omega) \left(T_b - (T_b - T_a) \cdot e^{-|\Delta\omega|/\Delta\omega_0} \right)$$

Main parameters in a Torque Converter

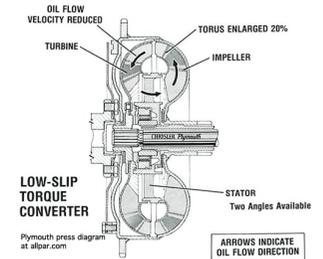
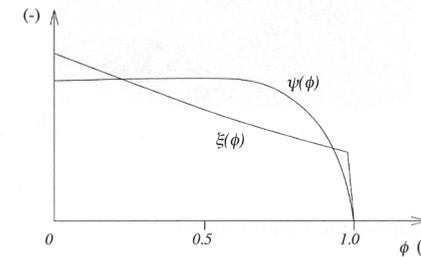
Input torque at the converter:

$$T_{1,e}(t) = \xi(\phi(t)) \rho_h d_p^5 \omega_e^2(t)$$

Converter output torque

$$T_{1,gb}(t) = \psi(\phi(t)) \cdot T_{1,e}(t)$$

Graph for the speed ratio $\phi(t) = \frac{\omega_{gb}}{\omega_e}$, and the experimentally determined $\psi(\phi(t))$



The efficiency in traction mode becomes

$$\eta_{tc} = \frac{\omega_{gb} T_{1,gb}}{\omega_e T_{1,e}} = \psi(\phi) \phi$$

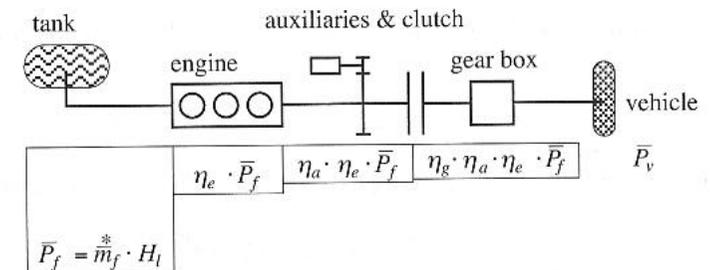
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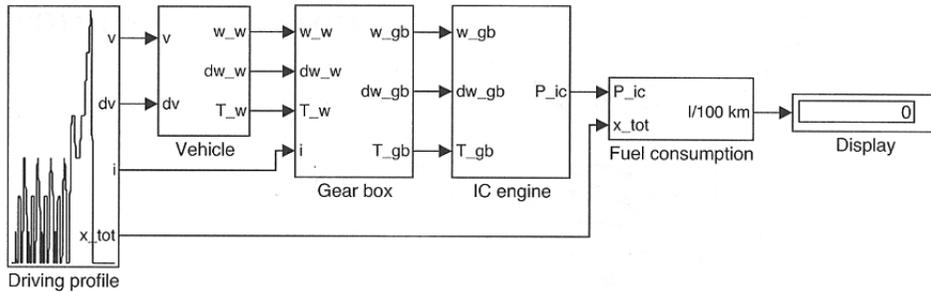
Average Operating Point Method



- Average operating point method
 - Good agreement for conventional powertrains.
- Hand-in assignment.

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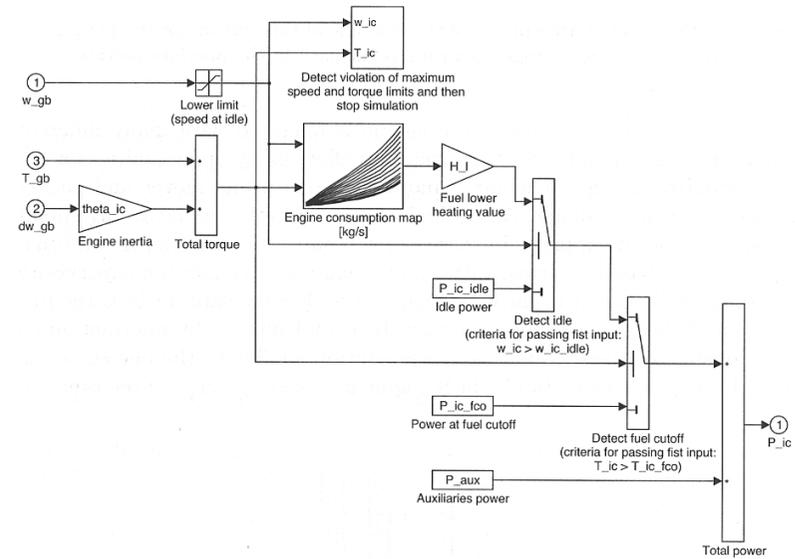
Quasistatic analysis – Layout



- More details and better agreement (depends on model quality)
 - Good agreement for general powertrains
- Hand-in assignment.

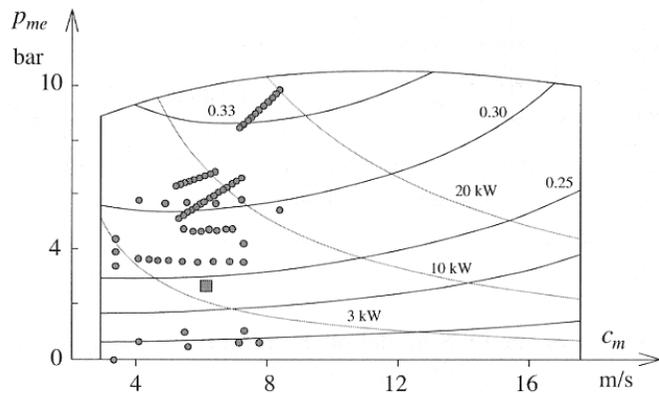
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Quasistatic analysis – IC Engine Structure



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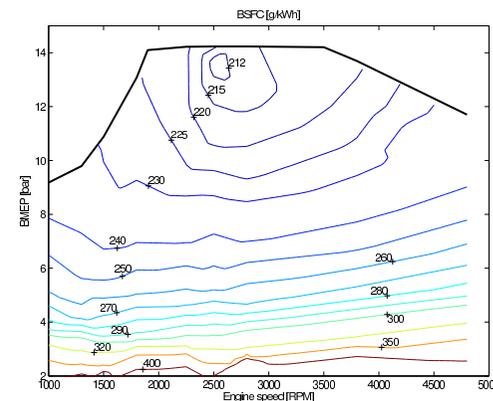
Quasistatic analysis – Engine Operating Points



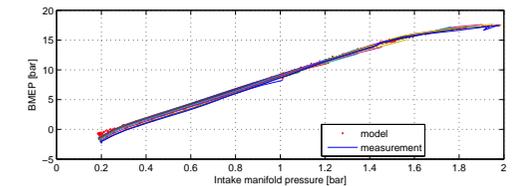
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Why is the average operating point surprisingly good?

The data looks quite nonlinear...



The Willans line approximation
– is surprisingly good for normal driving.



The average value from a process that has variations that follow a line will end up on the line.

If we avoid the extremes it becomes a good approximation.

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Performance and driveability

- Important factors for customers
- Not easy to define and quantify
- For passenger cars:
 - Top speed
 - Maximum grade for which a fully loaded car reaches top speed
 - Acceleration time from standstill to a reference speed (100 km/h or 60 miles/h are often used)

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Top Speed Performance

- Starting point – The vehicle motion equation.

$$m_v \frac{d}{dt} v(t) = F_t - \frac{1}{2} \rho_a A_f c_d v^2(t) - m_v g c_r - m_v g \sin(\alpha)$$

- At top speed

$$\frac{d}{dt} v(t) = 0$$

and the air drag is the dominating loss.

- power requirement ($F_t = \frac{P_{max}}{v}$):

$$P_{max} = \frac{1}{2} \rho_a A_f c_d v^3$$

Doubling the power increases top speed with 26%.

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Uphill Driving

- Starting point the vehicle motion equation.

$$m_v \frac{d}{dt} v(t) = F_t - \frac{1}{2} \rho_a A_f c_d v^2(t) - m_v g c_r - m_v g \sin(\alpha)$$

- Assume that the dominating effect is the inclination ($F_t = \frac{P_{max}}{v}$), gives power requirement:

$$P_{max} = v m_v g \sin(\alpha)$$

- Improved numerical results require a more careful analysis concerning the gearbox and gear ratio selection.

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Acceleration Performance

- Starting point:
Study the build up of kinetic energy

$$E_0 = \frac{1}{2} m_v v_0^2$$

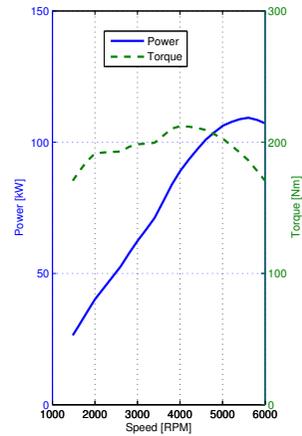
- Assume that all engine power will build up kinetic energy (neglecting the resistance forces)
Average power during acceleration: $\bar{P} = E_0/t_0$

- Ad hoc relation,

$$\bar{P} = \frac{1}{2} P_{max}$$

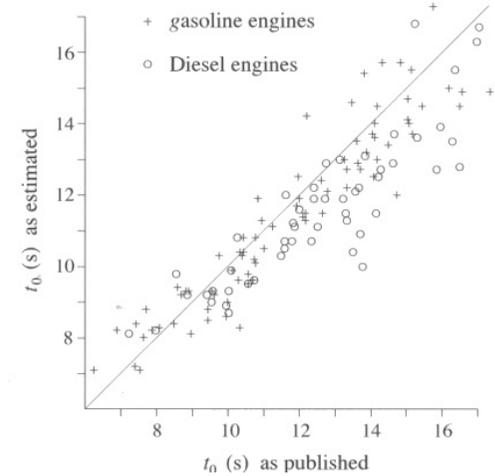
Assumption about an ICE with approximately constant torque (also including some non accounted losses)

$$P_{max} = \frac{m_v v^2}{t_0}$$



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Acceleration Performance – Validation



Published acceleration data

Compared to

$$P_{max} = \frac{m_v v^2}{t_0}$$

Surprisingly good agreement

Encourages us to make simplified models and analyses

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Optimization problems

Different problem types occur in vehicle optimization

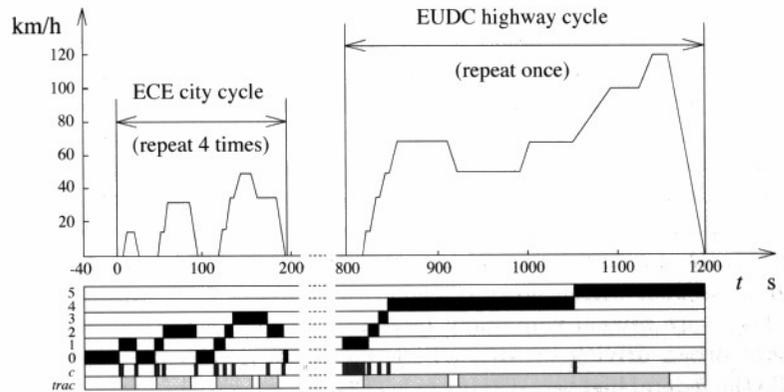
- Structure optimization
–What components to select and use?
- Parametric optimization
–What are the optimal design parameters?
- Control system optimization
–How shall the system be controlled?

Next up

Parametric optimization of the gear ratios in a conventional vehicle.

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Driving cycle specification – Gear ratio



Number of gears and their usage is specified, but ratios free.

–How much can changed gear ratios improve the fuel economy?

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Path to the solution

- Implement a simulation model that calculates m_f for the cycle.
- Set up the decision variables $i_{g,j}$, $j \in [1, 5]$.
- Set up problem

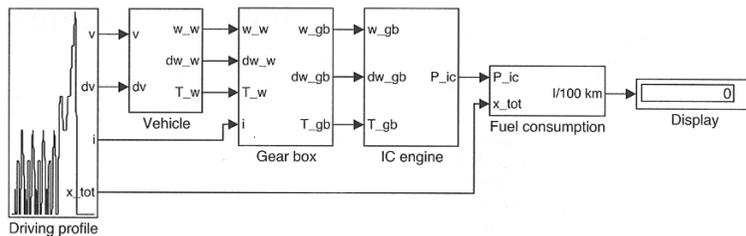
$$\begin{aligned} \min \quad & m_f(i_{g,1}, i_{g,2}, i_{g,3}, i_{g,4}, i_{g,5}) \\ \text{s.t.} \quad & \text{model and cycle is fulfilled} \end{aligned} \quad (1)$$

- Use an optimization package to solve (1)
- Analyze the solution.

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Model implemented in QSS

Conventional powertrain.

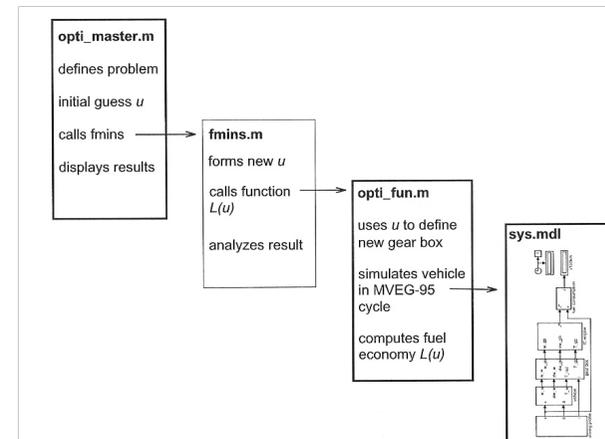


Efficient computations are important

The simulation model is evaluated many times while we search.

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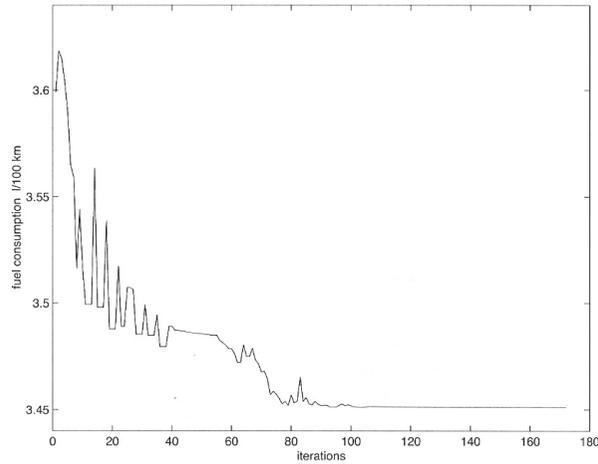
Structure of the code



Will use a similar setup, for a different problem, in hand-in assignment 2.

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Running the solver

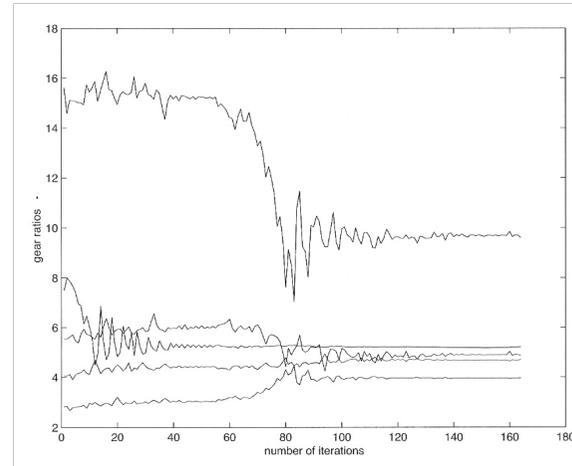


Improves the fuel consumption with 5%.

–Improvements of 0.5% are worth pursuing.

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Running the solver



Complex problem
–Global optimum not guaranteed.

Make sure you're not stuck in a bad local minimum.

Several runs with different initial guesses.

The optimizer shamelessly exploits all means it has.

–The solution is always an extreme point.

–Not necessarily good...

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Software tools

There are many tools for studying energy consumption of different vehicle propulsion systems

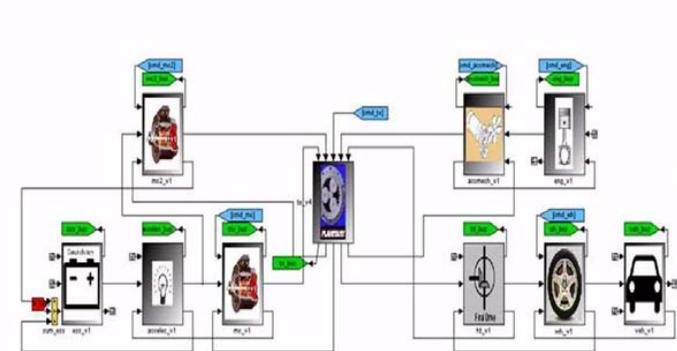
	Quasi static	Dynamic
QSS (ETH)	X	
Advisor, NREL→AVL	X	(X)
PSAT		X
ALPHA		X
VECTO		X
VSim (Volvo)		X
VTAB (Scania)		X
Inhouse tools	(x)	(X)

ALPHA – Advanced Light-Duty Powertrain and Hybrid Analysis. (EPA)

VECTO – Vehicle Energy Consumption calculation Tool. (EU, HD)

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PSAT – Argonne national laboratory



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Information from AVL:

- The U.S. Department of Energy's National Renewable Energy Laboratory (NREL) first developed ADVISOR in 1994.
- Between 1998 and 2003 it was downloaded by more than 7,000 individuals, corporations, and universities world-wide.
- In early 2003 NREL initiated the commercialisation of ADVISOR through a public solicitation.
- AVL responded and was awarded the exclusive rights to license and distribute ADVISOR world-wide.