# Fuel Level Estimation for Heavy Vehicles Using a Kalman Filter

Master's Thesis Performed in Vehicular Systems By

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# Fuel Level Estimation for Heavy Vehicles Using a Kalman Filter

Master's thesis performed at: Division of Vehicular Systems Department of Electrical Engineering Linköping University

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#### Sammanfattning/Abstract

The object with this project is to develop a more accurate way to measure the level in the fuel tank in Scania vehicles. The level should be displayed for the driver and a warning system be implemented to make the driver aware if the fuel level is too low. Furthermore a main goal is to develop an estimation of the distance that the vehicle could travel before refueling is needed.

The fuel level estimation system is modeled using Matlab Simulink and simulated with measurement data collected from real driving scenarios. After evaluating the system it is implemented in one of the electrical control units located on a test vehicle which communicates with other systems. After implementation more tests are performed with the test vehicle to verify that the same functionality achieved during simulations is achieved using the system implemented in a vehicle.

The fuel level estimated with a KF (Kalman filter) that uses fuel consumption and level measurement results in good performance. A more stable level estimate is achieved and a negative elevation of the estimate most of the time, as a result of fuel use. Compared to the method Scania vehicles estimate their fuel level with today the new level estimate is more steady and not that easily affected by fuel movements. The KF is more demanding in terms of memory allocation, processor speed and inputs needed, which has to be considered when comparing both methods. Another disadvantage with the KF is that it is dependent on the samples from the fuel level sensor to get an initial estimate during startup.

Furthermore the KF is easily expanded with more inputs that use information from other sensors on other parts of the vehicle.

#### Nyckelord/keywords

Kalman filter, distance estimation, fuel tanks

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The fuel level estimation system is modeled using Matlab Simulink and simulated with measurement data collected from real driving scenarios. After evaluating the system it is implemented in one of the ECUs (Electrical Control Units) located on a test vehicle which communicates with other systems. After implementation more tests are performed with the test vehicle to verify that the same functionality achieved during simulations is achieved using the system implemented in a vehicle.

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# Acknowledgement

Starting with some basic ideas how to combine different signals in a Scania vehicle to estimate the fuel volume this project resulted in a useful and implement able system. The main reason that made this project interesting was that I could perform all steps from ideas to implementation in a vehicle.

I would like to express my gratitude to Scania CV AB and the people working at the department RESK where my project was carried out. I have had a lot of freedom when developing and testing my ideas that led to the result that I have summarized in this report. Especially my supervisors Tobias Öberg and Andreas Jerhammar have given me support during the whole project and sharing their knowledge and experience with me. Beside the people working at RESK I have had personal contacts with several other people working at Scania that have helped me.

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Södertälje, November 2008

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# 1 Introduction

This Master's thesis project has been carried out at Scania CV AB in Södertälje at the chassis systems design department RESK. Scania delivers trucks, busses, marine and industrial engines to several parts of the world. The company aims to deliver the best trucks in the world by prioritizing quality and costumers needs. Most of the research and development takes place in Södertälje, Sweden.

## 1.1 Background

Up until now the accuracy of the fuel level measurement has not been of great importance. The purpose measuring the fuel level has been to present the information on the dashboard with a fuel level meter. Instead of accuracy the two most important things have been to avoid rapid changes in the fuel level displayed and the meter must indicate that the tank is empty when the fuel level is below a predefined level. To fulfill these requirements a fuel level sensor mounted inside the fuel tank is used. The sensor has a discrete numbers of levels and a table for the specific tank containing information about how much volume a specific sensor level corresponds to. The signal from the table is then passed through a first order exponential lowpass filter and displayed on the dashboard.

In cold environments like the northern parts of Sweden during winter the vehicle may not be turned off while refueling and the filter could cause a large time delay before the estimated volume reaches the true level. The filter is slow since it is designed to block all rapid changes caught by the fuel level sensor. If the truck is turned off during refuel it is not an issue since the filter is restarted when the ignition is turned on, with the current level from the sensor as initial output. If the truck is not turned off during refuel the filter is most likely much slower than the level change caused by a refueling. The driver will not see the total effect of the refueling on the fuel meter until the filter has caught up.

If functionality beyond presenting the fuel level on the dashboard should be implemented other goals will be considered. For example better fuel level measuring accuracy may be needed. A case when that accuracy may be requested is when estimating the remaining distance the vehicle is able to travel before refueling. Information about how far that distance is could be useful for truck drivers. The driver could fill the tank with the correct amount of fuel needed for the trip and the extra weight that excessive fuel gives could be reduced. Another way of using the estimate of the remaining distance is to combine the refuels with the rest and sleep that the driver needs to have in the schedule during driving.

This thesis investigates the possibilities of getting a more accurate fuel level estimate using the current hardware. The goal is to accurately estimate the fuel level and compare it to the fuel level estimation method currently used in Scania vehicles. Beyond the fuel level accuracy a way of separating a refuel from ordinary fuel movements is requested. This thesis also consider ways to estimate the remaining distance until the tank is empty based on previous and current driving conditions.

### 1.2 Limitations

There are both software and hardware limitations when implementing a system in a vehicle. Several ECUs (Electrical Control Units) are used on a vehicle controlling different electronic systems such as engine control, steering and cab ventilation. The fuel system has one sensor that measures the fuel level, which is connected to one of the ECUs in the vehicle. When the different systems are communicating across the vehicle a CAN-bus (Controller Area Network-bus) is used. The network has limits in bandwidth and signals cannot be achieved with maximum bandwidth because they share the network and have different priorities. For this project a separate ECU is added to the CAN-bus that is connected directly to the fuel level sensor. The ECU contains a programmable processor and input and output ports for communications. More information about the electronic hardware used is given in chapter 4.

This thesis mainly considers the types of fuel sensors and tanks used in Scania vehicles today but some alternatives are considered. Measurement data is collected from mainly three different vehicles and the system may behave different if other vehicles with other tank sizes are used.

The main problem when measuring the fuel level in a tank is the request to use as much fuel as possible from the tank before indicating that a refueling is needed.

When estimating the remaining distance the accuracy of the signals used is considered to be high.

### **1.2.1** Fuel movements in the tank

Vehicle movements give rise to different forces acting on the tank making the fuel move in ways that is hard to predict. The fuel could move in any direction depending on the forces and non-stationary fuel sloshing takes place. The sloshing increases when the amount of fuel decreases. This is a major limitation because it is when the tank is almost empty that finding the correct fuel amount left in the tank is most crucial (see ref. [7]). It is more difficult to determine the correct fuel level when the fuel surface is irregular caused by sloshing. The impact of fuel movements on the signal that measures the fuel level can be reduced by lowpass filtering it.

The fuel system has to be able to collect fuel while driving in different terrain e.g. steep road slopes but also when sloshing takes place. The minimum amount of fuel that have to be left in the tank (safety volume) to guarantee that fuel can be collected is calculated by using a test vehicle and drive in as many scenarios as possible. The amount of fuel in the tank is reduced until the limit is found when the vehicle can manage all extreme driving scenarios and still be able to collect fuel from the tank. A catch-tank system (see paragraph 2.1) could reduce the amount of fuel that has to be left in the tank.



Figure 1-1: 3D-drawing showing extreme fuel sloshing taking place in a tank. The dark mass indicates the fuel and the fuel pick-up is the gray cylinder at the edge of the mass.

### 1.2.2 Fuel containing water

If diesel fuel is used there is a small, yet considerable, amount of water in the fuel bought at gas stations. Some parts of the fuel system are sensitive to water and therefore it must be removed before it reaches these sensitive parts. A filter is used to extract the water from the fuel and the most common way is to gather the collected water into a container. The container is manually emptied when it is full. Water has higher density than the diesel which means that the water will sink to the bottom. Therefore the amount of water collected in the fuel system can be reduced by always leaving some fuel in the tank. But that does not correspond to the request of using as much as possible of the fuel in the tank. The safe volume left in the tank due to fuel sloshing covers this but if fuel should be collected below the safe volume level the water could be a problem. For more information about the problem with water see ref. [11].

### 1.2.3 Leakage

Leakage can occur if there has been some kind of damage to the tank, hoses or other parts of the fuel system. These leakages can be detected by using a diagnostic system but that is beyond the scope of this thesis. A possible leakage will not be taken into consideration and if such leakage occurs it will be considered as interference acting on the signal that indicates fuel use in the vehicle.

### 1.2.4 Sensor limitations

There are three main limitations for the fuel level sensors used. The first one is that the sensors used in Scania vehicles produced today are discrete with only up to 25 steps depending on tank height, secondly it cannot reach the last 9 centimeters to the bottom of the tank. Finally there is only one sensor that measures the fuel level at one location in the tank. The first two problems can be solved by using a different sort of fuel level sensor. With the current sensor only the second problem can be reduced by using information from sensors in other part of the fuel system e.g. the sensor that measures the instantaneous fuel flow into the engine. The solution to the third one is simply to add more sensors at other locations in the tank. The disadvantage doing this is that sensors are expensive. One more sensor in the tank could make it possible to detect for instance road slopes and adjust the estimated level according to that. The sensors are not

cheap and extra I/Os, cables etc. have to be added. Therefore if one more sensor should be added it must lead to a major improvement for fuel measurement and/or other functionality.

The longitudinal road slope is calculated in one of the systems in the vehicle but the lateral road slope is not. If both had been available the fuel movements could have been detected in a more accurate way. The road slope is used together with the fuel level sensor to evaluate the impact from road slopes on the fuel level.

In this thesis, model errors and disturbances that affect signals used from other parts of the vehicle are roughly estimated if no information about them is available.

# 2 Fuel system

The fuel system basically collects fuel from the tank and delivers it to the engine. For diesel engines with solid injection all fuel transported to the engine is not used instantaneously. The amount of fuel not used is lead back to the fuel tank. The reason is that the injectors should have at least the amount of fuel needed at all times. There could be other systems except the engine that use fuel from the tank, e.g. the cabin heater. The different systems that use fuel are described further in paragraph 4.3.

## 2.1 Fuel tank

The shape of the tanks differs between more or less cuboidal to cylindrical and each type of tank is produced in different sizes. Usually the tanks are long and little wider compared to the height, see Figure 2-1 for a sketch of a typical tank used on Scania vehicles. The tanks have plates with holes mounted on a couple of locations inside the tank to reduce the fuel sloshing. The other tank types used today are similar to the wide tank except for the cylindrical which has a circular cross-section.



Figure 2-1: Sketch of a wide tank.

Customers request larger tanks and therefore more complex shaped tanks may be considered in the future, that are able use the free space around the tank in a better way.

Except the tank types used in Scania vehicles today a regular tank with a catch-tank will be considered in this thesis. The catch-tank is simply a small extra tank that is less sensitive to fuel movements. For example it could be created by mounting a solid plate close to the end the tank or an extra tank outside the regular tank. The idea with a divided tank could be observed in Figure 2-2. This can hopefully reduce the amount of fuel that needs to be left in the tank before indicating that a refueling is needed. The benefits are both that the driver does not have to refuel as often and the weight of the vehicle is decreased.



Figure 2-2: Sketch of a tank including a catch-tank.

### 2.2 Fuel Pick-up

The fuel tanks have one pick-up device that collects the fuel into the pick-up system. If the catch-tank technique is used the fuel system needs to collect fuel from both tanks and the large tank could be almost empty before refueling. As mentioned earlier the system used today collects more fuel than needed and the excessive fuel is lead back to the tank. Using a catch-tank the fuel is lead back to the small tank which ensures that it is always filled. See Figure 2-3 for a picture on what the fuel pick-up looks like.



Figure 2-3: Fuel tank of Wide-type with armature containing level measurement and fuel pick-up devices. The sensor on the armature is the longitudinal type, described in paragraph 2.3.2.

### 2.3 Fuel Level Sensor

The most important part of the fuel system for this thesis is which type of fuel level sensor is used. In the past, Scania has used a float arm device for measuring the fuel level, but nowadays a longitudinal sensor is mostly common. In the future other sensor types may be used, an ultrasound distance-sensor is one suggestion for such a sensor. The sensors measure the fuel level by creating an electrical resistance representing the current fuel level in the tank. Furthermore the drop in voltage over the resistance is measured. More description of how the voltage is measured is written in paragraph 4.2. The voltage could be transformed into height or volume by using a table that specifies the height and volume that corresponds to each possible voltage. Every type of tank has its own table. In this thesis the voltage is transformed into volume when fuel level measurements are used in the implementation of the KF, see paragraph 3.3.

To read more about sensor types suitable for fuel level measurement see ref. [11].

### 2.3.1 Float arm

This armature uses a floating ball that indicates the fuel level with a resistance created where the arm with the floating ball connects to the armature. One advantage with this sensor is that it is continuous but on the other hand it has high electrical tolerance which gives low accuracy in the measurements. Except the tolerance another disadvantage is that it is very sensitive to physical contact since the arm that carries the floating ball is weak.



Figure 2-4: Drawing of floating arm armature. The pipes and the arm are cut at some locations to reduce the size of the image which is indicated with wavelike lines. The resistance is measured where the arm connects to the rest of the device.

### 2.3.2 Longitudinal

The longitudinal resistive armature works as an adjustable resistor giving different values for different positions of its floating device. Instead of being continuous as the float arm, this sensor

measures the fuel level in up to 25 discrete steps. The number of steps depends on the length of the armature that is limited by the height of the tank. Because there is a distance between each step, the sensor is less sensitive to surface movements when the true volume is close to the middle of one of the sensor steps. The electrical tolerance is much lower than the one for the float arm armature. Further analysis regarding the tolerance for this sensor could be found in paragraph 4.5. A sketch of this sensor can be observed in Figure 2-5.



Figure 2-5: Drawing of longitudinal measuring device. The black solid floats and follows the fuel level.

### 2.3.3 Ultrasound

The ultrasound sensor has a sender that creates a sound pulse that is reflected on the fuel surface. The reflected pulse is received by the sensor and the distance is estimated by knowing the speed of sound in air. Figure 2-6 shows the principle of ultrasonic measuring. The advantages using this type of sensor are that it is usually cheaper than the longitudinal and it has no mechanical parts that could wear out. The disadvantages are that the sound waves may collide and interfere if the fuel surface is non-horizontal or irregular which gives false measurements. The ultrasound sensors usually give a higher number of levels compared to the longitudinal sensor and more accurate information about the true volume in the tank could be achieved. On the other hand if more levels should be represented it may demand better electrical tolerance at the input pins where the sensor value is received from the sensor into the ECU it is connected to. To view one example of an ultrasound sensor see ref. [10].



Figure 2-6: A figure showing the principle of ultrasound distance measuring.

# 3 Estimation of fuel level

The system will be represented by a state-space model. When a state-space model, started with a true initial state has model errors and input interference the uncertainty of the states will increase more and more for each time step. The model itself is unaware whether the states represent the true physical behavior of the system that the model is built for. Measurements from sensors representing the states can be used to reduce the uncertainty. A KF (Kalman filter) has the strength of combining information from several sensors for estimating states in a state-space model. The filter uses the difference between estimated volume and the volume measured in the tank by the sensor. The tank model is a simple model and there is only one measurement sensor available, though the model can easily be expanded if more sensors are added in the future. All signals used by the KF model are considered to have SI units. For more information about state-space models see ref. [4] and for information about the KF see ref. [1].

### 3.1 Tank model

When modeling the tanks a simple approach is used with only one state representing the fuel volume, x=V, in the tank. The input will be the fuel flow u=q. The state space model makes it possible to implement a KF with the fuel level sensor as measurement signal, this is described below in paragraph 3.3.



Figure 3-1: Sketch showing a tank with a certain volume V(t) and a fuel flow q(t).

The model can be written as:

$$\dot{x} = f(x, u)$$
  

$$y = g(x, u)$$
(3.1)

When trying to decide the functions f and g in equation (3.1) the model is either built on known physical relationships or by Black-box modeling where the goal is to fit some mathematical expression as good as possible to measured data (see ref. [4]). In this case a physical model with simply an integration of the fuel volume flow is used which determines how much fuel that is

used. The system needs an initial state for the volume and after that it is driven by the fuel flow q(t).

#### 3.2 Time discrete model

The implementation of equation (3.1) is done in Matlab Simulink and it is made time discrete, for further information about Simulink see ref. [6]. The main reason for the discretization is that the implementation in the ECU needs a time-discrete representation. If the model is discrete from the beginning it is easier to use the model built in Simulink in the ECU implementation and the same behavior is achieved in both Simulink and in reality. The implementation is further described in chapter 4. The Euler method is used to approximate the derivatives (see ref. [4]). The result is described by the following expression using the sample time  $T_s$  as time step:

$$x(t + T_s) = x(t) + T_s q(t) = Ax(t) + Bq(t)$$
  
y(t)= x(t) = Cx(t) (3.2)

The unit for fuel flow input q(t) is m<sup>3</sup>/s resulting in that the output y(t) represents the current volume in the tank in m<sup>3</sup>.

Input signal q(t) may contain disturbances such as prediction errors and disturbances acting on the signal while it is transferred from its transmitter to the receiver. The signal is not measured with a sensor, instead there is a model that predicts the flow based on how long time the diesel injectors in the engine are active per engine cycle. Besides the disturbances from q(t) there is a model uncertainty caused by the discretization. The true fuel flow signal is called u(t) and the disturbances w(t) and the following model is achieved:

$$x(t + T_s) = Ax(t) + Bu(t) + w(t)$$
  
y(t)= x(t) = Cx(t) (3.3)

### 3.3 Kalman filter

Since the system defined by equation (3.2) is linear, it is guaranteed that the KF is the optimal filter if the disturbances in the process and measurement are described in a realistic way and are normally disturbed white noise. White noise has a mean value of zero and a constant variance. It is difficult to know the exact behavior of the real noises but the better they are described the better the filter will be. When designing this KF the disturbances are considered to be of normally distributed white noise character. This assumption has consequences, real disturbances are rarely of the mentioned character but it is a often a good approximation. Knowing that the state x(t) represents the fuel volume in the tank and that the volume is measured with a sensor, y(t), a KF can be used to estimate x(t).



Figure 3-2: Box schematics showing how the KF uses feedback of the difference between the estimated and measured value for the volume to control the state-space model.

When designing the filter the following notations are introduced:

- $x(t+T_s) \hat{x}(t+T_s)$  Prediction error
- P(t) Prediction error (co)variance (only one state)
- $y_s(t)$  Fuel volume measurement
- K(t) Kalman gain
- Q Process variance (for model and input noise)
- R Measurement noise variance

The fuel volume is not measured directly, the sensor measures the height in the tank which is transformed into the corresponding volume.

The KF algorithm for one time step prediction can be expressed in the following way:

$$\hat{x}(t+T_s) = A\hat{x}(t) + Bu(t) + K(t)(y_s(t) - C\hat{x}(t))$$
(3.4)

$$K(t) = AP(t)C^{T} (CP(t)C^{T} + R)^{-1}$$
(3.5)

$$P(t+T_{s}) = AP(t)A^{T} + Q - AP(t)C^{T} (CP(t)C^{T} + R)^{-1} CP(t)A^{T}$$
(3.6)

There is little information available for this thesis to estimate the process variance, because no interference model for the input q(t) is available. Engineers at Scania working with engine development says by experience that the momentarily error for the signal q(t) is  $\pm 10\%$ . Based on that the variance for the process error is estimated to be the square of 10% of the standard deviation for the fuel consumption signal. The standard deviation for the signal is calculated by

using the Matlab function STD on 1.75 hours (*N* number of values) of recorded signal data from regular driving with a Scania truck. The calculation is expressed as an equation further down. For more information about STD see ref. [6].

The sensor error variance is set knowing that the fuel sloshing can make the fuel sensor to vary up to 4 levels, found when analyzing driving scenarios (see Appendix A). During simulation 4 levels turned out to be too much and it was reduced to 3 to get a filter that relies slightly more on the fuel level sensor. The variance is set to the square of the volume that corresponds to 3 levels in the sensor for the specific tank used. The KF handles the pre-filtering itself by using little of the information in the feedback  $K(t)(y(t) - C\hat{x}(t))$  except during start up. In other words the feedback gain (Kalman gain) K will reach a small value because R >> Q.

The state will be initiated with the first value that comes from the sensor and the prediction error variance will be set based on the distance between each sensor step. The last mentioned variance indicated with P based on the assumption that the sensor may indicate one level too high or low when the algorithm starts.

The following summarizes the initial information for the KF:

. .

$$Q = \left(0.10 \cdot \sqrt{\frac{1}{N} \sum_{k=1}^{N} (u_k - \overline{u})^2}\right)^2;$$
(3.7)

 $\overline{u}$  – Fuel consumption arithmetic mean value.

$$R = (3 \cdot \Delta y)^2$$
;  $\Delta y - \text{Volume difference between sensor steps.}$  (3.8)

$$x_0 = y(0)$$
 (3.9)

$$P_0 = (y_{+1}(0) - x_0)^2; \ y_{+1}(0) - \text{Sensor level above } y(0).$$
(3.10)

Before the estimate  $\hat{x}$  is set to be the output of the model a function keeps the state within the limits of the tank. It is calculated with the following expression:

$$\hat{x}(t+T_s) = \min(\max(\hat{x}(t+T_s), 0), x_{\max})$$
(3.11)

The KF is defined by equation (3.4)-(3.6) and (3.11) and these equations are updated each time sample giving an estimated fuel volume  $\hat{x}$ .

When the filter starts its feedback gain is large and it is decreasing until the KF reaches steady state, see Figure 3-3. The effect of this makes the samples collected during the period of time until steady state has more impact on the level estimate than the sensor values after that. The filter has no information if the sensor values are trustworthy or not. Without functionality that detects if the sensor values are trustworthy or not the filter has to be adjusted as good as possible for all scenarios. The best assumption for this filter is that the samples collected from the time that the vehicle is started until the filter has reach steady state together represent the true initial volume. An example when that assumption gives a false initial state is if the vehicle was started when standing in a steep road slope and not reaching flat road until after the filter reached its

steady state. In that situation the filter could take long time until it reaches the true state because the feedback gain from the estimation error is small. An advantage is though that the bigger the estimation error is the bigger impact it has on the filter input, i.e. a faster change in the filter estimate.



Figure 3-3: Plot showing how the Kalman feedback gain slowly reaches its steady state during the startup period for the KF.

Since A and C given by equation (3.2) and R and Q are constants a stationary KF could be used. The stationary KF uses a pre-calculated feedback gain instead of letting equation (3.4)-(3.6) slowly find the correct gain. The effect of combining several samples during startup would be lost if the feedback gain is constant from the beginning. The filter behavior during the initial period until steady state is reached could be observed in the results presented in paragraph 3.5.1 and 4.6.

#### 3.4 Refuel detection

The KF needs a period of time to become steady. When the filter operates in steady mode it is suited for the regular behavior of its inputs, but if the inputs suddenly behave in a different way the filter may not work as requested. For example the filter may take too long time to reach the true state if a refueling is performed, approximately 20 minutes depending on which speed the tank is filled with. There are basically three ways that the fuel level sensor output behaves. First fuel sloshing is one way which makes the sensor output to vary up to 4 sensor levels. Second the truck may stand still and the level is steady indicating a constant level and finally is when refueling that causes the fuel level sensor to increase a period of time until the tank is filled. If the truck is turned off while refueling the filter will restart because the ECU is restarted. Though, if the truck is kept running the filter must be restarted in some automatic way. On option is to reset the filter as soon as the truck halts but this will cause the KF to lose all the information that the filter gathered so far, which is not good if the halt was not intended for a refueling. Instead a monitoring algorithm that detects a change in the fuel level sensor behavior will be used.

The algorithm is active while the vehicle stands still, it is assumed that the vehicle does not move while refueling. Some fuel movements may still take place in the tank when the refuel starts after a halt but they will not differ more than one sensor level. The sensor output is observed and if it increases 5 levels without exceptions an alarm is set, indicating that a refuel takes place. The alarm is used to reset the KF on and on until the vehicle starts moving again.



Figure 3-4: Sketch showing the idea of a detector controlling the KF.

### 3.5 Simulation results

The KF is implemented using Simulink where the systems are built by using blocks that represent mathematical functions and wires that transfers signals between the blocks. The block representing the state-space model is given by equation (3.4)-(3.11) with fuel consumption and sensor level as input. It also has an input from the detector which has a separate block with implementation of the detection algorithm described in paragraph 3.4. The detector also requires one more input, the vehicle speed. The estimate achieved from the KF is given in cubic meters and it is transformed into percent before it is set as output. One more block is added that represent the way that the fuel level is estimated on Scania vehicles today using a simple exponential filter. In this way both methods can be compared at all times. The Simulink model can be observed in Appendix B.

The input data used in the simulations is data recorded with different trucks. While simulating in Simulink all significant signals are recorded and later plotted to visualize how the two filters behave. Some results from the simulations are presented below.

### 3.5.1 Model and filter verification

The model is driven with recorded data from a driving scenario long enough to show a significant change in the fuel level. The sequence of recorded data is 67 minutes long and recorded when driving on highway with a Scania truck with a 625 liter tank and a 20 tons trailer. At first the model is driven only by the fuel consumption q(t) and the results can be observed in Figure 3-5 below. The model needs an initial state for the fuel volume and it is set by looking at the fuel level sensor start value, which indicates just above 40%.



Figure 3-5: Plot for model output driven by only the fuel consumption.

If the model input q is ignored and the estimation error from the KF drives the model alone the output shown in Figure 3-6 below is achieved.



Figure 3-6: Plot for model output when driven by only the error between the estimate and fuel level sensor.

If the KF alone controls the model the volume change is slower compared to if the model is driven with the fuel consumption. The KF has the strength of adjust the estimate towards the level measured with the fuel level sensor and the advantage with the fuel consumption is that it gives better information of how much fuel that is used by the vehicle without being affected by fuel movements in the tank. The resulting output when using both signals could be observed in Figure 3-7 below. The second plot shows what the discrete longitudinal sensor output is during the drive. The output bounces up and down caused by fuel movements but a pattern could be observed, the fuel level is decreased.



Figure 3-7: The first plot show when the model is driven by both fuel consumption and estimation error. The second plot is the fuel level sensor output for the drive cycle and the third the fuel consumption.

For this driving scenario the initial state used when simulating with fuel consumption was obviously too low which the KF compensates for by forcing the level to increase for a while from startup and then begin to decrease. Both Figure 3-5 and the first plot in Figure 3-7 indicate a rather constant level the last 400s. The reason for that is the low fuel consumption during that period of time that could be observed in the third plot in Figure 3-7.

#### 3.5.2 Refueling detection verification

The two following figures show the result of a fast refuel that took approximately 20s and a regular refill of a 625 liter tank that lasted for about 270s. The fast refuel that takes 20s is just a simulation where input data is created by modifying data recorded from a drive scenario to simulate the refuel. The other refuel is not modified, the model is driven with data recorded from a real refuel done with a truck.

First the algorithm output and its alarm level are plotted to show when the alarm is triggered. The KF and the exponential filter are compared to show the speed of tank detection compared to leaving the exponential filter to reach the true level on its own. KF continues to follow the sensor value until the vehicle starts moving again. A difference is that data used for the fast refuel simulates that the vehicle starts moving when the refuel is done, see Figure 3-8. The vehicle used during the real, slow, refuel remains at the same location during the whole measurement, see Figure 3-9. As mentioned in paragraph 3.4 the algorithm is not reset until the vehicles starts to

move again after the refuel. A signal named tank alarm indicates when the algorithm detects a refuel.

The robustness of the algorithm is tested by simulating different long data-series with recordings of signals used in the fuel estimation system. False alarms did not appear in any of the available recordings.



Figure 3-8: Plot showing how the refuel algorithm and KF reacts to a fast refuels. The refuel starts at 360s and goes on for approximately 20s. At 530s it could be observed in the second plot that the vehicle starts moving again and the refuel algorithm output is reset.



Figure 3-9: Refuel detection for a regular refueling of a 625 liter tank. The refueling starts at 50s and goes on for approximately 270s. The vehicle stands still during the whole time and the refuel algorithm is not reset.

### 3.5.3 Refueling compare

The KF output from both refuel scenarios shown in Figure 3-8 and Figure 3-9 are compared with how the regular exponential filter reacts to those refuels during simulation. The KF has the detection algorithm controlling it, which helps to reduce the time it takes for the estimated level to reach the sensor output. The outputs from both filters for the fast refuel could be observed in

Figure 3-10 and the comparison between both filter for the regular refuel can be observed in Figure 3-11.



Figure 3-10: Plot showing the outputs from KF with refuel detection and exponential filter without refuel detection during a simulation of a fast refuel that takes approximately 20s.



Figure 3-11: Plot showing the KF with refuel detection compared to the exponential filter without the detection functionality. The refilling of the tank is done at 320s.

### 3.5.4 Regular driving

First a regular driving that goes on for 4.8 hour is simulated with a couple of stops. The truck is driven on highway road most of the time. The truck has a 600 liter tank. At 10300s and 14700s the truck stops and the filter estimate is drawn towards the constant sensor level.



Figure 3-12: A plot showing the volume estimate from the KF and the raw data from the fuel level sensor.

Another long regular drive is presented below in Figure 3-13. It is an 11 hour drive with two stops. Again a 600 liter tank is mounted on the truck used. By looking at curves for such a long drive the exponential filter is less steady than the KF. There are two stops during the period where the engine is turned off but data is continued to be collected. The fuel level sensor then stops at the current level. Compared to the plots in Figure 3-12 the estimate is closer to the sensor value at the stops and the estimate is not drawn upwards, instead it is kept constant.



Figure 3-13: Plot showing the estimated volume from KF, the raw value from the sensor and the gain used in the feedback.



Figure 3-14: Plot that shows the output from the exponential filter usually used in Scania vehicles.

If a shorter segment of the data is observed there is a higher variation in the output of the exponential filter compared to the KF. At two occasions the sensor signal makes a sudden drop for several samples followed by it returning to the level above. These happen between 20600s and 20800s and between 21000s and 21200s which affects the estimate from the exponential filter a lot more than from the KF. The result for both filters can be observed in Figure 3-15.



Figure 3-15: Plot showing the fuel level estimate from KF and exponential filter for a segment of a recorded drive. The sensor output is also shown to get a view of the relation between all three signals.

#### 3.5.5 Validation Analysis

As the plots from the paragraph above visually indicate, the KF output gives a more steady level that is not easily affected by fuel movements. It is more difficult to validate the instantaneous value of the fuel level estimate. This KF sees the fuel level measurement far from perfect and instead relies more on the fuel consumption which would indicate less impact of fuel movements. In Table 1 there is a summary for a standard deviation test where the deviation for both filtering methods is compared. A number of driving scenarios are analyzed.

This analysis compares the STD (standard deviation) for the KF way of estimating the fuel volume with the exponential filter, which gives information about the degree of scattering for the filter outputs mentioned. Further the STD of the sensor is calculated to show how much of the scattering is removed by the filters by comparing the three STDs calculated. The signals are first detrended, which means that their mean values are subtracted from each sample to give a signal

that better show the signal scattering rather than how it deviates from its mean value. All calculations are done in Matlab using the functions named DETREND and STD, for further information see ref [6]. The following table present the result of STD calculations performed on a number of recorded driving scenarios.

	Driving scenario	Length	STD KF	STD Exp. Filter	STD Sensor
1	Driving mostly on highway.	2.8h	0.2713	0.4124	1.4515
2	Driving mostly on highway. (See Figure 3-12)	4.8h	0.3799	0.7295	1.4626
3	Driving on highway south of Södertälje, Sweden.	32min	0.1573	0.2446	1.8887
4	Driving with a small amount of fuel in the tank to see how the fuel movements affect the fuel level sensor. The vehicle is driven on a road known to contain certain road slopes and curves.	14.4min	0.1599	0.4327	2.8227
5	Similar scenario as nr 4.	8.7min	0.6991	0.5694	2.9378

Table 1: Summary of standard deviation for the filters and sensor for different driving scenarios.

Scenario nr 5 in Table 1 shows an occasion where the KF has a higher STD than the exponential filter. The reason for that is that the exponential filter fortunately had a good initial state and was not affected much from the fact that the sensor was varying a lot during the first 30s. The KF finds the level as the exponential filter but since the Kalman gain is high during those 30s the estimate was affected by the varying fuel level sensor. If the data sequence had continued for a longer period the impact of the first 30s would have been very small and the exponential filter would most likely have had a higher STD. The outputs from both filters and sensor could be observed in Figure 3-16 below.



Figure 3-16: Plot for fuel level estimation from both exponential filter and KF. The KF follows the fuel level sensor during startup.

Scenario nr 4 contains several slopes and at two occasions a long 16% road slope, between 567s and 593s and between 665s and 688s. The road slope is defined as the ratio between the vertical and the longitudinal rise expressed in percentage. The plots in Figure 3-17 shows the relation between the fuel level sensor and the road slope. The road slope caused the sensor to indicate 0% fuel level which affects the exponential filter output to decrease and increase again when the road slope is passed. There is a time delay until the road slope clearly affects the estimate caused by the filters.

The KF is not affected that much, just a slight decrease could be observed when the road slope is significant.



Figure 3-17: Plot for a drive scenario taking place on test track with defined road slopes and curves.

# 4 Implementation in a vehicle

For testing of the KF a new ECU is added to the CAN-bus to minimize the interference with other systems.

### 4.1 Communication

The CAN-bus handles the communication between ECUs in the vehicle. All the sensors on the vehicle are connected to the ECUs and the values are both used locally in the ECU and send over the network to other parts of the vehicle. Signals calculated in ECU could in a similarly way be shared over the network.

The CAN-bus was first invented with the aim to reduce the weight of the electrical system in vehicles and to create one uniform communication standard. Another advantage is that it is easy to connect new devices to the network without affecting the current setup. The CAN-protocol defines the serial communication between ECUs using a bus network. Scania uses the SAE J1939/11 standard which transfers up to 250kbits/sec in the CAN physical layer. A PC could be connected to the network and achieve information from the bus. The PC can also be used the other way by sending information and flash the different ECUs with new software.

The data on the CAN-bus is read from an external PC using a hardware interface and there are several software programs that could be used to process the data. The raw data could be displayed and logged by having a database which defines how the data should be transformed to achieve physical values from it. One example of a hardware that could be used is named VCI (Vehicle Communication Interface). For this thesis the VCI is used for flashing the added ECU described in paragraph 4.4 and to read information using the GUI described in paragraph 5.2.

Different software use different ways of communicating with the CAN-bus and one useful program is CANalyzer made by Vector, which makes it possible to monitor and record data from CAN, for documentation see ref. [9]. In this thesis CANalyzer is used to record data during testing in a vehicle and the results are presented in paragraph 4.6. A laptop with a CANcard is connected to the CAN-bus via a special cable called CANcab.

### 4.2 Measuring fuel level

When the resistance varies in the level sensors (described in paragraph 2.3) it results in a variation in the voltage signal which can be observed and used in the fuel level measuring system. The ECU has a constants resistor  $R_2$  and voltage 5V at the input pin. The resistor  $R_2$  is connected in a series circuit with the variable resistor  $R_1$ , see Figure 4-1.  $R_1$  is not variable in a continuous sense, instead it has its limited number of values for the specific sensor used.  $R_1$  represents the resistance given by the fuel level sensor and the voltage U can be calculated with equation (4.1) below. The variable resistor has a tolerance of  $\pm \Delta R(R_1)$ . The longitudinal and most commonly used sensor in Scania vehicles has the lowest relative tolerance when it reaches the bottom of the tank where the accuracy is most important. More details about the tolerances could be found in paragraph 4.5.

$$U = 5V \frac{R1}{(R1+R2)} \left[ V \right] \tag{4.1}$$



Figure 4-1: Schematic showing how the fuel level sensor voltage is measured with the signal U.

The voltage achieved from the sensor is then passed through a look-up table that gives a fuel level matching the input voltage for the specific tank type used. The table gives the volume level for the voltage level closest to the input. A look-up table with *n*-values looks like this:

$$V(U) = \begin{cases} V_1, & U = U_1 \\ V_2, & U = U_2 \\ \vdots \\ V_n, & U = U_n \end{cases}$$
(4.2)

The diagram in Figure 4-2 shows a typical relation between sensor voltage and tank volume for the longitudinal sensor.



Figure 4-2: A diagram showing the relation between sensor voltage and tank volume for a 600 liter wide tank and 300 ohm resistance R2.

### 4.3 Measuring fuel use

The engine uses the majority of the fuel collected from the tank by the fuel system. In addition there is a cab heater that could be used to heat the air in the cab while the engine is cold or turned off. The engine uses fuel when combusting it to mainly produce work and the heater combusts fuel to produce heat. There are three different types of heater, two of them heat the air directly (ATA) and the last one heats water that circulates in the engines cooling system (WTA). The water then heats the air in the ventilation system for the cab. The cabin heater has 4 different power stages (25%, 50%, 75% and 100%) when it is turned on. The maximum fuel consumption is given by  $c_i$  for the different types of heaters. The following yields for the heaters considered:

 $q_c(t) [m^3 / s]$ -Fuel flow entering the cylinders.

$$q_{h}(t) = \begin{cases} c_{f}, heater \ on \\ 0, heater \ off \end{cases}$$

$$c_{f} = \begin{cases} <3.67 \cdot 10^{-7} \ m^{3}/s, WTA - heater \\ \leq 7.78 \cdot 10^{-8} \ m^{3}/s, ATA - heater - Fuel \ flow \ used \ in \ heater. \\ \leq 1.42 \cdot 10^{-7} \ m^{3}/s, ATA - heater \end{cases}$$

One occasion then the cab heater is used is when the vehicle is turned off and the driver rests inside the cab and then nothing can be done with the signals because the ECUs are off. The heater is also often used if the engine is cold, recently started and there is little cargo. In that case it can take long time for the engine to become warm and another heating source, besides the engine, is required during that time.

When analyzing records of fuel consumption for trucks driving long distances the mean value for engine consumption usually is about 30L/h. Based on that consumption the largest heater consumption shown above corresponds to approximately 5% of the total fuel consumption.

If the truck is left with its engine idling and cabin heater on, a larger fraction is used by the heater. In that case the cabin heater consumption might be a significant part of the total fuel consumption depending on power state. When the engine idles the fuel use is around 1.8L/h and the largest heater consumption then corresponds to 42% of the total fuel consumption. Because the cabin heater could represent a significant part of the fuel consumption it has to be added to the engine consumption and together they represent the total fuel consumption.

### 4.4 Rapid prototyping

Scania has developed an interface for using model based development (RPS-system) which generates C-code from Simulink models. The code could be implemented in a special type of ECU for which the RPS-system is designed for. When implementing the new fuel level system this system is used.

There are some limits with the ECU used with the RPS-system, both processor speed and memory is limited compared to a modern PC which has to be in mind when implementing the code. Input pins can be read every 10ms and the ECU is also connected to the CAN-bus to communicate with other parts of the vehicle. The speed that the CAN-messages can be read with is limited by how often the senders update their output of the messages. The tolerance for the ECU input pins is  $\pm 20$  mV caused by the A/D-converter. The tolerance could cause a bias fault

when measuring the fuel level sensor voltage. If the longitudinal sensor is used the distance between each sensor step represents 80-270mV, which gives an idea of how much the input tolerance can interfere.

The RPS-system demands a constant sample time to be set before compiling the model, which is 10ms. Some predefined Simulink blocks in the RPS-system used for communication with the vehicle demands this sample time.

When the fuel level is calculated in the added ECU it can send the value via the CAN-bus to the dashboard in the cabin so the driver can see it. The ECU that handles the instrument in the cabin is named ICL (Instrument Cluster). Normally an ECU named COO (Coordinator) handles the fuel level measuring and sends the result via the CAN-bus to the ICL. While testing the new system the added ECU overrides the fuel level measured by COO and controls the dashboard fuel level indicator. The signals of interest on the bus can be observed in a PC. While testing, several signals from the fuel level estimating system are send over the CAN-bus to be able to monitor how the system behaves.



Figure 4-3: Sketch showing the systems communication with the CAN-bus. The box named RPS is the new ECU mounted for testing the new fuel level system.

### 4.5 Tolerances

There are both electrical and mechanical tolerances affecting the fuel level measurement. Electrical tolerance involves cables, connectors, A/D-converting and other components used to transfer the electrical signals. The mechanical tolerance comes from differences between sensors and how they are mounted in the tanks. In this paragraph the longitudinal sensor is considered.

If all worst case tolerances are put together all the way from level measurement to level estimate the total tolerance can be calculated. The schematic in Figure 4-1 indicates that there is a constant voltage source of 5V, which is not true at all times. Because the voltage varies the A/D-converter needs to keep track of how much it differs from the wanted 5V. The voltage is indicated with Uref and it is measured to get a better accuracy for the input. When knowing the difference between Uref and 5V the A/D-converter compensates for a possible error. The converter has a tolerance that affects U and it is specified to be maximum  $\pm 20$ mV.



Figure 4-4: Schematic showing how the voltage from sensor is measured (U) with resistances that affects it.

Except for the input pin resistor  $R_2$  and the sensor resistor  $R_1$  there is a resistance caused by cables, connectors etc. named  $R_c$ . At Scania this cable resistance is considered to be between 0-1 $\Omega$  that is based on a standard calculation where each connector could add 5 m $\Omega$  and the cables 26 m $\Omega$  per meter.

The longitudinal sensor output varies between 42  $\Omega$  (top of tank) and 2794  $\Omega$  (bottom of tank) for the longest sensor used. The possible values for all resistances are summarized in Table 2.

Resistance name	Value $[\Omega]$	Max. Tolerance
R1	(42,,2794)	±(1Ω+1%)
Rc	0-1	0
R2	750	±1%

Table 2: Summary of resistances involved in measuring fuel level.

There are two extreme cases for each sensor level, the first occurs when  $R_2$  reaches its maximum tolerance while  $R_1+R_c$  reached their minimum tolerance and the second case occurs is the opposite when  $R_2$  reached its minimum and  $R_1+R_c$  its maximum tolerance. The two cases are considered for the highest and the lowest value achieved from the sensor. This gives a total of four extreme cases. If the A/D-converter tolerance of  $\pm 20$ mV is added a total of 8 possible cases that will be considered.

In the model used the sensor values are sent into a look-up table which transforms them from voltage to volume. The table consists of the predefined levels calculated for the tank type used. The table uses the predefined volume level for the predefined voltage level closest to the input voltage. This means that the table will send out the correct level as long as the input stays closest to the true level.

When calculating total electrical tolerance it is found that the voltage into the ECU may vary between 230mV and 300mV in the top of the tank where the defined level is 270mV. The closest level is the second from the top and it is defined as 380mV. Since 300mV is closer to 270mV than 380mV the electrical tolerance will not be a problem for this case.

At the bottom of the tank the voltage input into the ECU may vary between 3900mV and 3980mV where the defined level is 3940mV. The closest level is 3807mV, which means that the tolerance will not be a problem here either.

The mechanical tolerance is given in distance and it is  $\pm 2$ mm and the sensor is usually 585mm long. This tolerance can never be avoided and there is always a risk that the true level is 2mm lower or 2mm higher when changing from one level to another.

Test runs shows that the filter works good but the tolerances has to be kept in mind, the sensor level could not be trusted at all times.

### 4.6 Test drive results

C-code is generated by compiling the system implemented with Simulink blocks. The filter is represented in the same way as in Figure B.1-1 in Appendix B. To send and receive the signals involved some more blocks are added to handle that communication. The added ECU is flashed with the code and connected to the vehicle. Every interesting signal from the system is send over CAN from the ECU and recorded with software in a PC. Several test runs where performed with the ECU in a Scania truck. The outputs from the ECU were observed to analyze the filter behavior online and some recordings are presented below.

The first driving scenario is the same as the one used in the verification paragraph 3.5.1. The system implemented in the ECU gives similar results except the resolution is reduced to 0.4%, which makes the output behave in a less continuous way compared to the simulation result. The model itself has high resolution but the signals send over the CAN-bus has lower resolution which affects the recorded data. The outputs from the KF and exponential filter could be observed in Figure 4-5 below.



Figure 4-5: Plot showing the fuel level estimate from both the KF and the exponential filter.

Similar results are achieved for every type of driving scenario when comparing the ECU output and the simulation results in Simulink. This indicates that the model works properly when it is implemented in a Scania vehicle.

# 5 Fuel functionality

If the current fuel volume and fuel consumption is available, the distance left before a refuel is needed could be estimated. The functionality is implemented with Matlab scripts and the information is presented in real time using a GUI on a PC. Data is collected from the CAN-bus into the PC, using a VCI. The method used for estimating the distance is simple and neglects possible errors in the signals used.

### 5.1 Estimating distance before refuel is needed

To be able to estimate the distance the vehicle is able to travel before the tank is empty, the mean value of the fuel consumption and the current fuel volume in the tank is needed. The fuel consumption will be expressed as distance travelled per liter fuel for the vehicle so far since start or since a major cargo weight change. The momentarily consumption for the engine and cabin heater is available on the CAN-bus and the distance travelled is achieved by looking at the total distance travelled by integrating the velocity.

When designing the fuel functionality the following notations are introduced:

- s(t) Distance travelled [m]
- v(t) Current vehicle speed [m/s]
- c(t) Current fuel consumption [m<sup>3</sup>/s]
- m(t) Vehicle weight [kg]
- C(t) Distance travelled per volume of fuel since start or major weight change [m/m<sup>3</sup>]
- $C_m(m(t))$  Distance travelled per volume of fuel during start-up period [m/m<sup>3</sup>]
- $\hat{V}(t)$  Estimated fuel volume in the tank [m<sup>3</sup>]
- $\hat{d}(t)$  Estimate of distance left before refill [m]

The calculation of C(t) needs a period of time to stabilize and during that time the fuel consumption per distance is set based on what a truck usually consumes given the current cargo mass. It is simply a linear interpolation between consumption and cargo mass based on measurement data. The interpolation output is named  $C_m(m(t))$  to indicate that it depends on the current cargo mass. The start-up state is kept until 30 seconds after the vehicle starts moving. During that time the integration of consumption and distance are stabilizing more and more for each time step.

The following equations defines the calculations performed when estimating the remaining distance:

$$s(t) = \int v(t)dt \tag{5.1}$$

$$C(t) = \begin{cases} C_m(m(t)), & \text{startup state} \\ \frac{s(t)}{\int c(t) \, dt}, & \text{otherwise} \end{cases}$$
(5.2)  
$$\hat{d}(t) = C(t) \cdot \hat{V}(t)$$
(5.3)

Sometimes the vehicle could be loaded or unloaded without turning it off. If a major weight change occurs the consumption calculated up until that moment in time may not represent the upcoming consumption in a good way. Every 10 minutes the vehicle mass is checked and if it changed by more than 10% since start or last major change the estimation is restarted, with startup state, and the vehicle mass is updated.

The switch from start-up state to normal mode could make the estimate change rapid from one level to another, which would be annoying for the driver. A slow exponential filter is used to filter the signal given by equation (5.3). During the last 50km of estimated distance left the filter is made faster. The filter with output l(t) is given by the following equation:

$$l(t) = \alpha \cdot l(t-1) + (1-\alpha) \cdot \hat{d}(t), \quad \alpha = \begin{cases} 0.95, \quad \hat{d}(t) < 50km \\ 0.999, \quad \hat{d}(t) \ge 50km \end{cases}$$
(5.4)

### 5.2 Graphical user interface

The GUI is created with Matlab Guide and presents information about current vehicle weight, fuel volume, distance remaining until the tank is empty, distance traveled since started and distance traveled since a significant change in weight. The functionality and visual look is created with scripts in Matlab and the program can be build into an executable program that runs on any PC. For more information about Matlab Guide see ref. [6].



Figure 5-1: Flow chart showing how the GUI works for fuel functionality

Everything that happens in the GUI is controlled by a timer and during every sample new information from CAN is received and decoded. The decoding is followed by calculations of time-discrete versions of equation (5.1)-(5.4). The discretization is done with the Euler method, see ref. [4]. The communication with the vehicles CAN-bus is done via a VCI by using a library file in the PC that defines how the data is achieved. The data collected consists of the raw values and have to be converted to real physical units using a database that defines how the signals are coded. Some of the outputs from equation (5.1)-(5.4) are converted into other suitable units before presented in the GUI.

The information is presented with formatted text that updates every sample. The GUI also contains a vertical bar that indicates the fuel level. When the level is below 5% the bar changes color from green to red and starts to flash to make the driver aware of the low fuel level. The menu contains different options such as to specify the maximum tank volume and a plotted curve of the fuel level could be observed in real time.



Figure 5-2: A figure of what the fuel functionality GUI looks like.

If a major weight change is detected and the algorithm is restarted, the estimated distance before refuel could make a major change instantly from one level to another. The weight change is indicated by a symbol that will appear on the GUI and stay visible for a period of time to make the driver aware of the reason for the sudden change in estimated distance left.



Figure 5-3: A figure that indicates a major weight change.

### 5.3 Test runs

The fuel functionality is tested while driving by connection a PC laptop to the CAN-bus and observing the GUI while the truck is driven. The data from the bus is at the same time recorded and further analyses are done by replaying it with a PC. Most of the information displayed in the GUI is directly decoded from CAN but the estimate of distance left before refill is interesting to analyze. Results show that the functionality works as requested but the estimation of the distance per liter fuel often takes a period of time to be stabilized. The filter helps to give a soft transit when the estimate changes from the constant one based on vehicle weight and the estimated distance left based on the collected data online. Figure 5-4, Figure 5-5 and Figure 5-6 shows some outputs when the functionality is tested with recorded data.



Figure 5-4: Plot showing signals for estimating the distance left until refuel.

The plots shows that the filtered estimated distance left, l(t), starts by following the estimate based on vehicle weight,  $\hat{V}(t) \cdot C_m(m(t))$ , and after the start up period it changes input to  $\hat{d}(t)$ . The filter is slow and not easily affected by the scattered behavior from l(t).

If the signal is continued to be observed the consumption stabilizes more and more over time. It still has scattering behavior caused by changes in consumption per distance travelled. The following plots in Figure 5-5 show the same scenario as Figure 5-4 but more data is used and the filter output together with the fuel economy (distance per liter) and fuel level are plotted. Since the fuel level is steady compared to the fuel economy the resulting distance left,  $\hat{d}(t)$ , mainly follows the fuel economy behavior.



Figure 5-5: Plots showing some outputs from the fuel functionality algorithm. The behavior of the estimated distance left follows the one for fuel economy.

Another scenario is recorded and replayed with the GUI. This time the consumption is higher than normal during the first 1000s that cause the filter output, l(t), to be drawn towards the short estimated distance left until it stabilizes and the filter output increase again. The estimate achieved during this scenario is presented in Figure 5-6 below.



Figure 5-6: Plot showing the estimated distance left. Both raw and filtered data are presented.

# 6 Summary & Conclusions

The KF relies mostly on the fuel consumption and little on the fuel level sensor except during startup. If high accuracy in the fuel consumption signal is achieved at all times this signal could alone represent the total decrease in fuel volume in the tank. However the estimate needs some kind of support since the fuel consumption is not trustworthy at all times and an initial state must be set. The support is achieved by using information from the fuel level sensor.

The exponential filter used today in Scania vehicles has the advantage of being simple and needs only one input. The KF needs at least two input signals; fuel level and fuel consumption. If the fuel is consumed by several systems the model may need one input from each system. If the level sensor values collected during startup give false information about the fuel volume the exponential filter will faster forget that information than the KF. This is due to that the filter relies more on the level sensor values during startup compared to its steady state. Steady state is reached within the first 3-4 minutes. Without better functionality to set the initial state the KF could present a fuel level with less accuracy than the exponential until the KF has compensated for its estimation error.

As the simulation results show, the KF is not easily affected by fuel movements in steady mode and the filter output rarely show a false increase in fuel level compared to the exponential design. The increase in estimated fuel level from the filters occurs when the level sensor has been giving false information about a certain fuel level for a while. Since the KF is less dependent on the fuel level sensor the false behavior is reduced when looking at the KF estimate.

Except visually validation of the fuel level estimate another way of measuring how steady the outputs from the filters are is by comparing their standard deviation. The KF gives a steadier estimate with less deviation than the exponential. One exception is if the data sequence is short and the KF estimates a bad initial state.

The refuel detector shows good performance and could be used to reset the KF. There is a small time delay until the detector finds the refuel behavior in the signal from the level sensor. The KF gets a signal from the detector and the filter is reset until the refuel is completed, which makes the KF output to follow the fuel level sensor rise. The detector is not limited to be used on the KF and the same detector could reset the exponential filter.

One problem with the fuel functionality that estimates the distance left until refuel is to have a good initial estimate. The initial estimate is presented for the driver until the estimation functionality have had some time to gather information to create a steady estimated consumption. The current way is done by predicting the initial estimate based on the vehicle weight and interpolate among mean consumptions achieved during test runs. This gives an estimate with a correct magnitude but without good accuracy until after several minutes from start when the calculation of the fuel economy based on sensors has stabilized.

Since the longitudinal fuel level sensor used today only has 25 steps to measure the fuel level it would be useful to have a sensor with more levels. The ultrasound sensor that was considered in paragraph 2.3.3 has more levels than the longitudinal. The extra steps achieved from this sensor may not be useful since there could be a lot of disturbances caused by the electrical and mechanical tolerances. All worst case tolerances have to be considered before deciding if the extra levels are valuable.

### 6.1 Conclusions

Both types of filters have their advantages and disadvantages. The following advantages and disadvantages are found for the KF compared to the exponential filter.

Advantages:

- Steady fuel level estimate.
- Combines fuel information from two signals.
- Not as dependent on the fuel level sensor in the long run.
- Easily extended with more inputs if more information regarding the fuel volume is added.

Disadvantages:

- Needs longer time to find the true estimate if the fuel level sensor gives false values during start up.
- Demands more input signals, memory and processor usage.

When looking at both advantages and disadvantages the KF is a good choice of filter if the steadier level estimate is worth the extra demands in computational power. It is probably not worth it for the fuel level meter on the dashboard, but if the fuel level is used in some other system that sees the estimation as accurate it is good to have a steadier level.

The fuel functionality shows one way of estimating the distance left without rapid changes, which is good if the result should be presented for a driver who usually prefers slow changes on the instruments. The disadvantage with the method is that it has no information about the fuel consumption to come. But it might be a first step to get a good estimate to make the driver aware of how long until a refuel is needed. This information makes it possible to plan his or hers drive and avoid driving with too much fuel in the tank. Further the driver could plan the drive in other ways, for example combining the breaks and sleep periods with the refueling. By doing this the driver could save time by not having to make more stops than necessary.

# 7 Further development

The basic KF is developed, which combines information that affects the fuel volume in the tank but more investigations can be done. Most important is to validate the instantaneously value of the fuel level estimate. If this can be done the startup parameters such as fuel level sensor variance could be adjusted to get as good accuracy as possible with the signals currently available. This validation could be done by measuring the fuel flow collected by the fuel pick-up device and the flow of excessive fuel that comes back from the engine. The flow meters must have good accuracy.

Since one of the disadvantages using the KF is that it could take long time to compensate for bad startup, some functionality that estimates the initial state is requested. When the vehicle has been going for a long period of time there is a lot of information gathered to estimate the current state and all this information is lost when the truck is turned off. By saving the state this information could be used the next time the vehicle is started. This gives rise to other problems because a lot of things could have affected the fuel volume in the tank during the time the vehicle was turned off. For example the tank may be refilled with fuel and then this have to be detected in some way when the system starts.

A way to expand the tank model with KF is to add a state which represents the current bias fault in the sensor depending on road slope, vehicle acceleration etc. Since the fuel moves as a result of road slopes and forces that raise from accelerations the information from the fuel level sensor could be processed in a different way when the fuel movements are detected. If a model could be found which estimates the sensor bias fault, current sensor value could be compensated for this and the resulting value could be more accurate. In this case the variance for the sensor could be decreased, which result in a faster filter.

The implementation of the KF in the Simulink model could be optimized by using other types of blocks when building it. The memory and processor usage has not been taken into account when designing the filter and several things can be done to optimize it.

The KF is adjusted to data collected with the three specific vehicles used during this thesis. If more data is collected for vehicles with smaller and larger tanks the system can be tested with that data. This makes it possible to investigate if the system needs adjustments depending on tank type or if it works fine with every type of tank that Scania use.

Tank leakage is something that would affect the fuel level and if such a leakage could be detected the driver must be informed and the vehicle should be taken to a workshop as soon as possible. Since there are two signals available that measures the fuel volume use, it is possible to design a diagnostic system that detects a fault somewhere in the fuel system, maybe a leakage. Methods presented in [5] could be used to create this system.

When dealing with fuel functionality the problem to have a good initial estimate could be reduced by saving the mean consumption from the last run. If this estimate is used instead of the one based on cargo weight it could give a better initiation since it is based on the individual truck that the system is implemented in. Beyond getting a good initial state the fuel functionality needs more testing to validate the results with.

Another useful work would be to investigate what professional truck drivers request when it comes to fuel functionality. What kind of functionality that the majority find useful could be achieved by interviews, handing out forms with questions etc.

A way to affect the estimated distance left is to use look-ahead information based on maps with information about differences in altitude on the road ahead. This could predict the consumption to come. The planned route ahead could be received from example a road navigator, if the destination is set.

The safety volume that needs to be left in the tank limits the amount of fuel that could be used. A catch-tank (see paragraph 2.1) will probably reduce this limited volume. Further work could be done to investigate if the catch-tank is a good idea and if the catch-tank affects the fuel volume measurement in any way.

If another type of fuel level sensor should be used it has to be investigated if the advantages with the sensor are useful. It may be at least as important to reduce the tolerances affecting the signal from the sensor to the receiving ECU.

# 8 References

All references to all material used in this report are presented below.

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### 8.4 Personal contacts

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# Notations

C-code	Code written in C programming language
ATA	Air -To-Air heater
WTA	Water-To-Air heater
Simulink	MathWorks SIMULINK
RPS	Rapid Prototyping Solution
ECU	Electrical control unit
CAN	Controller area network
GUI	Graphical User Interface
COO	Coordinator
ICL	Instrument Cluster
VCI	Vehicle Communication Interface
KF	Kalman Filter
STD	Standard deviation

# Appendix A Driving scenario analysis

This appendix presents the result for the different test drives performed to analyze the reaction in fuel level to different movements of the vehicle. Several test drives were done to analyze the impact on the fuel level when driving in defined scenarios. For every plot in this appendix the fuel level raw value is plotted, which is measured from the top of the tank. The changes of fuel level up and down can be a result of that the fuel level is about to change from one discrete level to another but the basic behavior can be analyzed

### A.1 Up- and downhill

When driving in road slopes the fuel level is affected and the sensor shows less fuel in the tank when driving uphill. For the type of tank used in the measurements presented in Figure A.1-1 below, the sensor value moves 2-4 levels which are approximately 5-10cm for this type of sensor in a wide-tank.



Figure A.1-1: Plots showing how the fuel level sensor reacts when driving uphill.

### A.2 Hard turns

When making turns the fuel level increases or decreases depending on which direction the vehicle turns and where in the tank the sensor is mounted. When turning left, see Figure A.2-1 below, the forces acting on the vehicle makes the fuel to displace to the right inside the tank. The sensor indicates more fuel then there is when turning left. At the end of the turn the fuel moves fast back to the left side of the tank which results in a lower level from the sensor then it started at. If the measurement period had been longer the level would had eventually go back to where it started.



Figure A.2-1: The figure shows how the fuel sensor reacts when a truck makes a sudden left turn.

## A.3 Hard accelerating and braking

When accelerating from zero the fuel level varies a lot because tank sloshing occurs and waves are created. When the vehicle stops accelerating and starts braking the sensor value varies more rapidly because of the change in direction of the forces acting on the vehicle. The result in presented in Figure A.3-1: below.



Figure A.3-1: The plots are showing fuel level sensor output and vehicle speed when accelerating and braking.

## A.4 Rocky road track

When driving on a straight rocky road track the fuel level sensor varies about 1-5 levels which represents 1-9cm for this sensor and tank type. The result is presented in Figure A.4-1 below.



Figure A.4-1: The plots show the impact on the fuel level sensor when driving on a rocky road track.

### A.5 Circles

In this scenario the vehicle is driven with full steering to the left followed by full steering to the right. When driving in circles the sensor shows less fuel while turning left and more fuel when turning right. That behavior indicates that the sensor is located on the right side of the tank used when measuring. The difference between the highest fuel level when turning right and the lowest fuel level when turning left is 6 levels or 13cm for the sensor used. Results can be observed in Figure A.5-1 below.



Figure A.5-1: The plots show a left turn circular driving followed by right turn circular driving.

## A.6 Urban environment

When driving in urban environment the fuel level changes at most 3 levels or 6cm. The result is presented in Figure A.6-1 below.



Figure A.6-1: The plots show 900 seconds of driving in urban environment.

# Appendix B Simulink model

This appendix presents the Simulink model used when simulating with recorded data. The same model is expanded with blocks for communication with CAN (Controller Area Network) when implementing the model in an ECU (Electrical Control Unit). Figure B.1-1 shows how the model is built in Matlab Simulink.

## B.1 Simulink fuel level estimation system



Figure B.1-1: Simulink schematic for the system used when simulating.